Controlling the polarization of segnetoelectrics while increasing the specific power and specific energy of the powertrain to increase the idle speed and reduce the charging time of electric vehicles

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Abstract: - This article discusses a small-size installation created using ferropiezoelectric ceramics to generate additional electricity. The use of an electrochemical generator in the unit makes it possible to increase the efficiency of electricity generation by controlling the polarization of ferropiezoelectric ceramics and applying innovation. At the consumption of 1 joule of electricity (using mechanical energy), 2...4 joules of electricity are generated at the output. The technology of increasing the energy is realized in two stages: the first stage increases the degree of polarization of the ferroelectric element, and the second stage increases the electrical power supplied to the load. The efficiency of the electrical installation is about 55...60 percent and depends on the modification of the ceramic and the electrical circuit.

Key words: - Reorientation, solid solutions, domains, energy, polarization, technology, batteries, electric transport
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1 Introduction

Studies of two-component systems of piezoceramic materials based on lead zirconate titanate (CTS) have led to the development of two-, three-, four-, and five-component systems [1]. Such high-performance materials exhibit segnetoelectric properties and elevated Curie temperatures (Tc).Four-component systems of complex lead-containing piezoceramic materials with significantly higher electrophysical and mechanical characteristics than the two-component CTS system are widely used in industry. However, despite significantly improved characteristics, these multicomponent materials (segneutoceramics) are unfortunately still not used to generate additional energy. They are used (as well as previously developed CTS systems) in energy conversion devices: piezotransformers, piezosensors, piezofilters, piezomodulators, etc.

Probably, the prevailing notion that it is inexpedient to use CTS systems for obtaining additional energy due to their low electrophysical and mechanical characteristics is automatically (subconsciously) "transferred" to these more efficient materials as well.

2 Factors determining the control of polarization in obtaining additional energy

One of the main features of materials with the piezo effect is a rigid temperature range in which their piezoactive properties are manifested. The upper point of this interval is Tk.

Segnetoelectric perovskites exhibit polymorphism depending on temperature, that is, their cube-shaped cell is distorted in various ways. Basically 3 forms or phases are used: tetragonal (T), rhombic and rhombohedral (Re), Figure 2. The boundaries between these temperatures are called phase transitions [2, 3]. These boundaries are "blurred" for many physical characteristics. As established [1], for four-component systems of solid solutions, the "blurring" in concentration transitions between tetragonal and rhombohedral phases is 2-5% of the change in titanium concentration along a certain section with promising material properties for it. This "blur" is denoted as the morphological region (MO). The reorientation polarization P_r (the number of domain reorientations remaining after removal of the electric field at preliminary polarization of the segnetoelectric) is important when selecting a segnetoelectric [1], just as K_p is the mechanical

activity. The excess energy is achieved by controlling the polarization of the segnetoelectric, which is determined by the choice of operating temperature range and frequency range and basically boils down to the following:
-choice of segnetoelectric material and circuitry for its inclusion in an electrical circuit;
-Selection of the frequency range and operating temperature range.

Figure 1 shows the K_p, P_r, d_{31}, g_{31} and $\mathcal{E}/\mathcal{E}_0$ curves. The figure shows that for the temperature interval corresponding to the rhombohedral segmented phase, the values of K_p, P_r , d_{31}, g_{31}, and $\mathcal{E}/\mathcal{E}_0$ are practically stable. P_r, d_{31}, K_p, and g_{31} significantly decrease in the transition to the tetragonal phase. $\mathcal{E}/\mathcal{E}_0$ is minimal, which corresponds to an increase in K_p , and increases during the transition to the tetragonal phase. It follows from the graphs that the maximum electromechanical activity of the K_p and the piezoelectric coefficient d_{31} depend on the residual polarization P_r and the relative permittivity $\varepsilon/\varepsilon_0$. These parameters of the crystals of the same name are in dependence:

$$K_p = 2\sqrt{\frac{2}{1-\sigma}}\sqrt{\frac{\varepsilon_{33}^{\mathrm{T}}}{S_{11}^{\mathrm{E}}}} \cdot Q_{12} \cdot P_r , \qquad (1)$$

where Q_{12} is the coefficient of electrostriction; (σ and S_{11}^{E} are Poisson's and pliability coefficients, respectively), $\varepsilon_{33}^{\mathrm{T}}$-dielectric permittivity.

σ is the Poisson's ratio and is a reference value. In calculations of devices using piezo- and segnetoelectrics, as a rule, σ = 0.24 - 0.4 depending on the chemical composition.

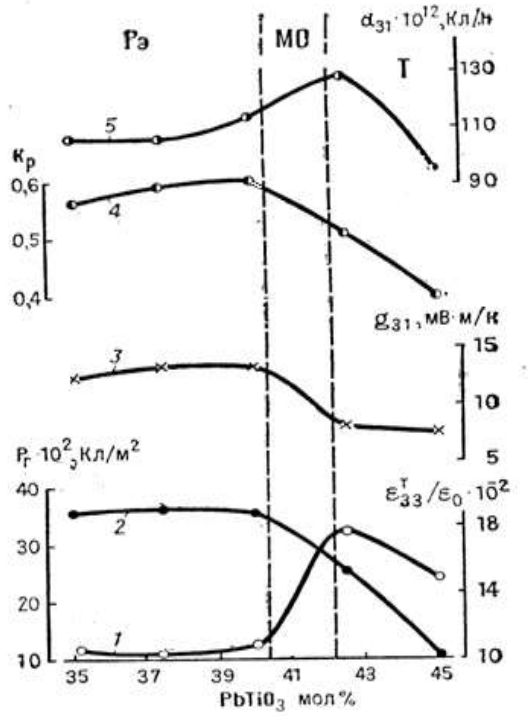

Figure 1. Composition dependences $\varepsilon_{33}^{\mathrm{T}}/\varepsilon_0$ (1), P_r (2), g_{31} (3), K_p (4), and d_{31} (5) for the system PbTiO3 - PbZrO3 – $PbNb_{2/3}Mg_{1/3}O_3$ – $PbNb_{2/3}N_{i1/3}O_3$.

Thus, the mechanical activity of K_p is sensitive to P_r and its maximum is in the rhombohedral region, which is defined for the crystals of the same name by a certain temperature interval near MO , i.e., the interval of operating temperatures t_p. The MO can be analyzed, for example, by means of concentration-temperature (C-T) phase diagrams, figure 2 [1].

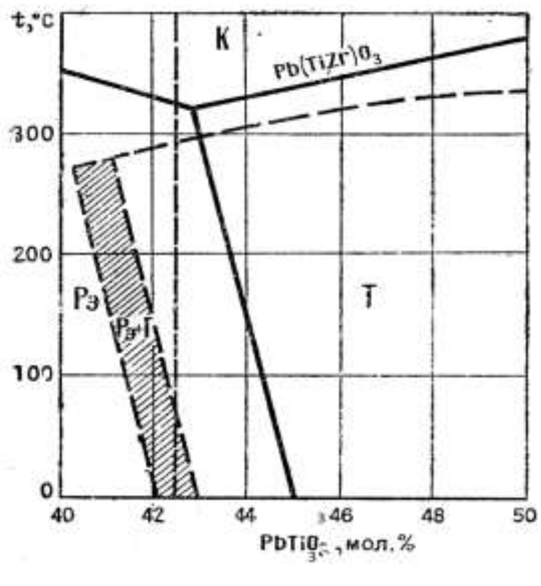

Figure 2. Phase diagram (C-T) of the system $PbTiO_3$ – $PbZrO_3$ – $PbNb_{2/3}Ni_{1/3}O_3$ – $PbK_{1/2}Mn_{1/2}O_3$ (dashed lines). The solid lines correspond to the CTS system

The figure shows the slope of the MO toward the rhombohedral phase for a four-component system of the form [1]: $PbTiO_3$ - $PbZrO_3$ – Pb $B'_{1-\alpha}$ $B''O_3$ - Pb $B'''_{1-\beta}B''''_{\beta}O_3$, где α(β) = 1/2,1/3,1/4 depending on the valence of the cations B′, B″, B‴, B⁗.

The cations that provide segnetoelectric properties can be the chemical elements Sb, Li, Bi and others of a certain valence.

The slope is determined by the concentration of the titanium-containing compound PbTi O_3 in a given solid solution of the four-component system. And the concentration of PbTiO3 in solution is correlated with the phase transition temperature.

Thus, for example, 41% of PbTi O_3 corresponds to approximately 110^0C of the segnetoelectric. The composition of the rhombohedral phase near the MO, as the temperature increases, transitions through the MO to the tetragonal T phase and then to the cubic K (paraelectric cubic) phase. This is explained by the fact that at large (critical) concentrations of titaniumTi near the MO, its atoms tend to stably shift . Therefore, the whole system tends to move to the tetragonal phase through the MO. As a result, the shape and volume of the cell change.

It was found [1] that the maximum number of residual 71^0 - degree domain reorientations of P_r is in the rhombohedral phase. The orientation is determined in the direction perpendicular to the sample surface It is known that the values of maximum reorientation polarization PR and residual PR are part of the spontaneous polarization of the Ps domains and are determined by the sum of all domain rotations and the polarization process. As a result of studies the degrees of domain reorientations under the action of electric field and residual, after removal of the field were determined.

It was also found [1] that the fraction of 71^0 – degree maximal (and also residual) reorientations in the rhombohedral phase with respect to Ps is approximately 86% (P_r ≈ 0.866). Figure 3(b) shows domains of P_s oriented spontaneously (less than 20%) and domains of P_r oriented at approximately 71^0 angles to the crystal surface (over 80%).

As mentioned above, the reorientation domains in the rhombohedral segnetophase are oriented at an angle of 71^0. In addition, the piezoelectric moduli in segnetoelectrics, which characterize changes in electric polarization under the action of mechanical loads, reach large values in the phase transition region (rhombohedral), increasing K_p, Figure 1. 71^0-degree domains under the action of mechanical loads, reducing the angle, reduce the residual deformation, Figure 3, and strengthen the local electric field inside the dielectric E_l, lining up along it.

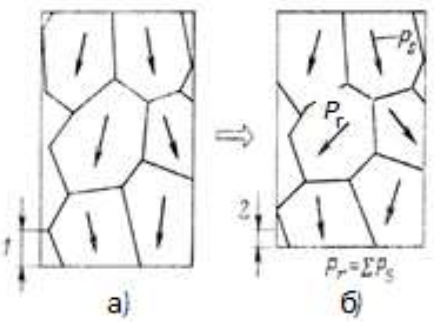

Figure 3. Ceramic polarization process. a - electric field is applied; b - after removal of electric field; 1 - electrostriction [3] deformation ; 2 - residual deformation; P_s - spontaneous (spontaneous) polarization [3]; P_r,-, oriented polarization.

Thus, the electric energy of the segnetoelectric increases W: W =-$\mu_d \cdot E_l \cdot \cos Q$ [3], where μd is the dipole moment, Q is an angle equal to approximately 71^0, figure 4.

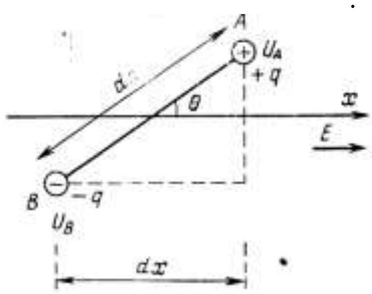

Figure 4. To calculate the domain energy possessed by the dipole moment
q - charges; Ua and Uв - charge potentials, d_s - distance between charges.

The local electric field in a segnetoelectric induced by charges generated under the action of mechanical loads can be significant and exceed the external electric field.

The increase in the local electric field E_l is also promoted by another piezoelectric modulus g_{31}, figure 1. The maximum g_{31} is shifted to the rhombohedral region and characterizes the tension

E_l arising under the action of mechanical stresses T, in accordance with the dependence E≈ -g·T [3].

Thus, by varying the concentration of the titanium-containing compound $PbTiO_3$ in the system of solid solutions of multicomponent segnetoelectrics, it is possible to control the t_p of devices based on them and to reach the maximum value of Kp.

Assume that a ferroelectric ceramic plate serves as an electromechanical transducer and creates compression oscillations along its length, Figure 5. To create a mathematical model it is necessary to develop the equation of motion of the transducer, to select the equations of the piezoelectric effect, and to make basic assumptions. The basic assumptions are as follows:
- all mechanical stresses, except those in the direction of the transducer, are zero;
- the amplitude of alternating mechanical stresses and strains does not exceed the maximum limiting values;
-the change in the reactive component of the transducer impedance at operating frequencies has a capacitive character.

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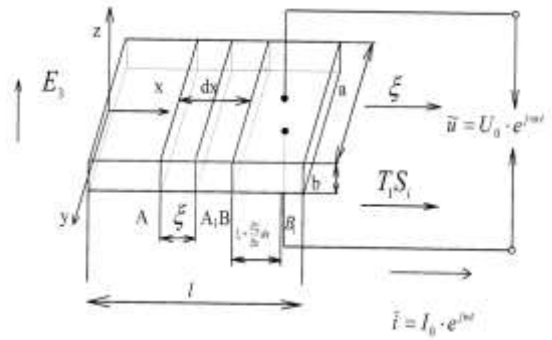

Figure 5. Diagram of the electromechanical transducer in interaction with ECG.

The equation of motion of the transducer is:

$$\frac{\partial^2 \cdot \xi}{\partial \cdot x} = \frac{1}{\nu^2} \cdot \frac{\partial^2 \cdot \xi}{\partial \cdot t^2}, \quad (2)$$

where ξ is amplitude of oscillation (displacement);

$\nu = \sqrt{\gamma / \rho}$ - speed of elastic wave propagation in the plate;

γ - modulus of elasticity of ferropiezoelectric ceramics;

ρ-ferropiezoelectric ceramics density;

l, a and b - length, width and thickness of the plate, respectively;

t- time.

This is a well- studied partial differential equation of second order.

The equation of motion of the transducer is solved by variable separation method:

$$\xi(x,t) = X(x) \cdot T(t),$$

$$\frac{1}{X(x)} \cdot \frac{\partial^2 x}{\partial x^2} = \frac{1}{\nu^2} \cdot \frac{1}{T(t)} \cdot \frac{\partial^2 T}{\partial t^2} = -n^2 \quad (3)$$

The solutions are the following, respectively:

$$X = A \cdot cos\, nx + B \cdot \sin nx,$$
$$T = C \cdot \ cos\, n\nu t + D \sin n\nu t = M \cdot cos(n\nu t + \varphi),$$

where $n = m \cdot \pi / 1$ (m = 1,2,3 ...). (4)

The resonance and antiresonance oscillation frequencies of the ferro-piezoelectric plate are determined for a fixed transducer. The boundary conditions are written as follows:

$$\xi(x,t) = X(0) \cdot T(t) = 0,$$
$$\xi(x,t) = X(l) \cdot T(t) = 0, \quad (5)$$

where l is length of the plate. Omitting the intermediate calculations shown in [4, 5], we present the unknown expressions for f_r and f_a.

$$f_r = \frac{1}{4 \cdot l} \cdot \sqrt{\frac{Y_{11}}{\rho}} kHz, f_a = f_r \left(\frac{K_c^2}{2.46} + 1 \right) = \frac{1}{4\,l} \left(\frac{K_c^2}{2.46} + 1 \right) \cdot \sqrt{Y_{11}/\rho},\ kHz \quad (6)$$

Thus, resonant and antiresonant frequencies can be approximated, which is important for calculating power plant specifications.

If an alternating electric voltage is applied to a segmented dielectric, the polarization does not follow the electric field, which leads to dielectric losses. When a mechanical load is applied, the deformation is established with a delay. That is, these processes correspond to a phase shift. All materials are subject to relaxation processes to a greater or lesser degree. Relaxation processes in ferroelectrics appear due to mechanical and dielectric losses. The peculiarities of ferropiezoelectrics of ferroelectrics operating in the dynamic mode is the presence of both types of losses. At low frequencies, the angles of dielectric and mechanical losses in it make a total loss angle δ, defined through K_c [3-7], see equation (7). Therefore, the polarization is considered as a complex number: $\varepsilon_{rk} = \varepsilon_r - j\, \varepsilon'_r$, where ε_r is relative dielectric constant; ε'_r - imaginary part of the complex number, loss coefficient ($\varepsilon'_r = tg\delta \cdot \varepsilon_r$); tgδ - loss characteristic: δ - phase shift angle.

The frequency characteristics ε_r, ε'_r and δ depending on the normalized frequency ω/ω_0 are as shown in figure 6.

Now it is possible to explain ECG operation principle in more detail. Under mechanical load, as a result of the clamping of ferroelectric, there is a sharp decrease in ε_r, figure 6, which leads to electrical capacity reduction and an increase in K_c, that is, to a sharp increase in the efficiency of conversion of mechanical energy into electrical energy. In a certain frequency range between the resonance and the antiresonance, where the deformation will increase sharply to a greater extent than is due to mechanical load, a sudden absorption of mechanical energy occurs. This leads to a sharp increase in the degree of polarization.

Reducing the electrical capacitance of the ferroelectric ECG leads to an increase in the electrical voltage U_O, see equation (8), and, therefore, an increase in the electrical power in the load EU. Phase transitions in ferroelectrics occur within certain temperature ranges. In this connection, it should be noted that in ferroelectrics some piezoelectric moduli, characterizing the change in the degree of polarization under mechanical loading, reach very large values during phase transitions, theoretically passing into infinity. Thus, the effect of mechanical load in a certain frequency range and the effect of thermal energy in a certain temperature range are a sort of a catalyst of chemical reactions in solid solutions of ferroelectrics and mainly increase the specific power and specific energy of the ECG.

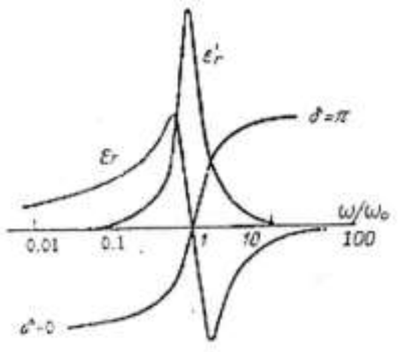

Figure 6. To the analysis of ECG resonance parameters.

The absolute dielectric constants, ε_α^S of the clamped element in this case are, of course, less than ε_α^T of the free one and are linked by equation of electromechanical coupling:

$$\varepsilon_a^S = \varepsilon_a^T \left(1 - \frac{d^2}{s^E \varepsilon_a^T} \right) = \varepsilon_a^T \left(1 - Kc^2 \right) \quad (7)$$

where K_c is electromechanical coupling coefficient, S^E is elastic compliance while the electric field strength is E=0, ε_α^T is absolute dielectric constants where the mechanical stress is T=0 and d is piezoelectric module [3-5].

In the general case, the transformation function (ECG) is of the form:

From equation (7) it is obvious that the value of K_c has a significant effect on the ratio of dielectric constant of clamped and free ferroelectrics, i. e change in the dielectric constant under the action of mechanical load. For example, in case of $K_c = 0.5$ (an averaged value), this ratio will be 0.75. Which, in its turn, is highly important (especially since in modern ferropiezoelectric ceramics $K_c = 0.6...0.7$ for output electricvoltage (output power) of the power plant, see equation (8), as dielectric constant and electrical capacity are directly proportional.

$$U_O = K_u \frac{d_{ij} \cdot F}{C_{ECG} + C_L}, \quad (8)$$

where U_O means output electric voltage of ECG, F is acting mechanical force, C_{ECG} is electrical capacity of ECG, C_L is electrical load capacity (load electrical devices), K_u is coefficient of electric voltage increase due to the increased degree of polarization of ferroelectric and d_{ij} is piezoelectric module, induced polarization per unit of mechanical stress.

3 Applying technology to generate additional energy

The mass transition to electric vehicles will require a large amount of additional electricity and the creation of networks of chargers and charging stations. To solve this problem, a power supply unit (EU) for slow, fast, and accelerated battery charging has been developed as a battery charger and charging station using polarization control of segnetoelectrics. Polarization control creates a technology to reduce energy consumption by changing the compressibility and electroelasticity of segnetoelectrics [3 ,7-10]. As a result, additional energy is released that is 2.5 to 3 times greater (depending on the segnetoelectric modification and inclusion in electric circuits) than the energy consumed from an alternating electric voltage source. This additional electrical energy is also the result of the second kind of segnetoelectric transition, migration and dipole polarization.

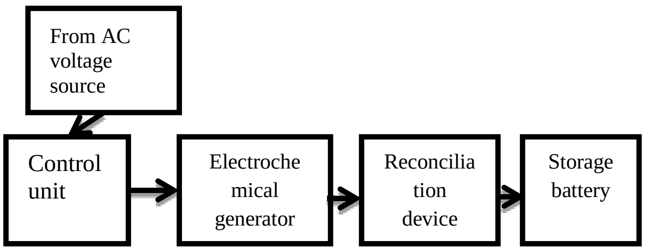

Figure 7. Functional diagram of the EU for charging.

The range of an electric car on a single charge is much less than the consumer needs. Its energy source (batteries) weighs a lot and is expensive. The reason is that the energy density of modern batteries is too low. Although the energy density of batteries has recently increased, they still weigh a lot, are large and expensive. The known simple ways to increase the energy density of batteries have all but been exhausted. In order for batteries to replace traditionally used internal combustion engines, their energy density must be increased by a factor of about 10. The use of solar and wind energy is still inefficient. In addition, the national interests of hydrocarbon-producing countries are a deterrent to the development of electric vehicles. Thus, the problem of battery energy needs to be solved. Toyota's solid-state batteries, which promise to greatly increase energy density, are still under development. And it could be a decade or more before these batteries become mass-produced. With this in mind, an innovative small-scale alternative powertrain (EU) technology has been developed that uses an electrochemical generator (ECG) based on ferropiezoelectric ceramics and provides a simultaneous increase in power density and specific energy. The unit also includes a mechanical energy generation unit and an electromechanical converter figure 8. The energy consumption of 1 joule when using mechanical energy makes it possible to obtain 2.5...4 joules of electrical energy at the output. The mechanical energy used is produced by a device of simple design. The unit also includes a device for obtaining mechanical energy and electromechanical converter figure 8.

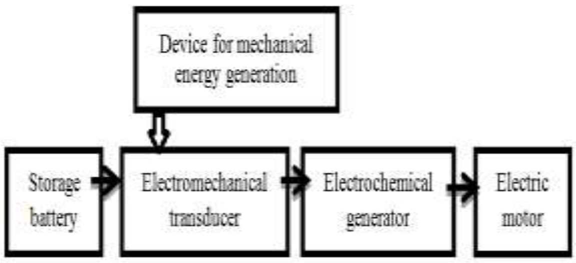

Figure 8. Functional diagram of the EU.

4 Dependence of the EU mass on the electric power it generates

Theoretical and experimental studies [5-7, 11, 12] showed that an increase in the electrical power in the load (P_L) by 2 times leads to an increase in the ECG mass (M_{ECG}) by $2\sqrt{2}$ times, by 3 times - by $3\sqrt{3}$ times and etc. In other words, these changes occur according to the law of geometric progression. And electromechanical converter and device, which generates mechanical energy (Figure 2.) increase this mass by 2,12...2 times. Thus, the mass of the power plant (without battery and electric motor) makes 2.12...2.2. M_{ECG}.

Figure 6 shows the growth-increase diagram of the $M_{ECG} - P_L$. The above the diagram makes it possible to calculate the mass of the EU (without the battery and electric motor) taking P_L into account. You can find a point on the diagram where P_L = 1.89 kW and M_{ECG} = 0.83 kg, near which P_L and M_{ECG} change almost directly in proportion. The M_{ECG} grows slower below this point and faster above it.

M_{ECG}, kg

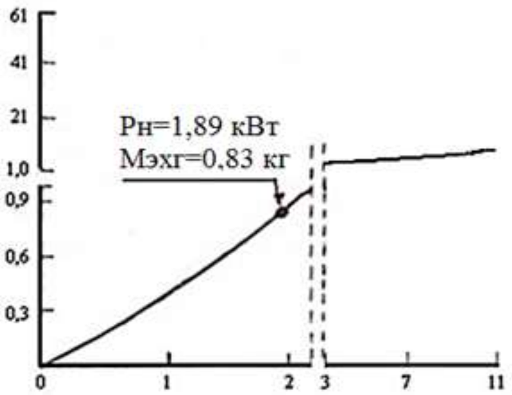

Figure 9. $M_{ECG} - P_L$ growth-increase diagram.

Figure 10 shows the character of the electrical voltage change for ECG at frequencies below resonance, where the oscillator resistance can be considered purely capacitive [5].

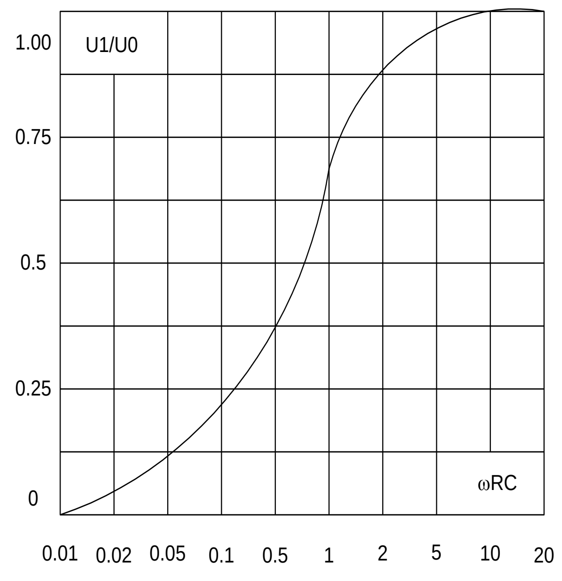

Figure 10. Frequency response of ECG.

U_O - this is the amplitude value of the voltage that appeared on the capacitance C at $R \rightarrow \infty$.

U_1 - voltage proportional to the change in mechanical load F, (8).

The curve in Figure 10 is a part of the experimental amplitude-frequency response of the electromechanical transducer made of the ferroelectric material PZT-19, diameter 10x1 mm with a mechanical load of 2.5 MPa (see in [4], Figure 4. 1, curve 2), in the frequency range between antiresonance and resonance. Depending on the nature of the electrical load of the EU (reactive or active), the scheme of connection and consumption of electrical energy changes [4,5]

5Conclusion

The proposed alternative innovative technology for obtaining additional energy compared to solar and wind technologies has an advantage: it does not depend on climatic conditions and time of day and has a high efficiency. The use of the developed EU due to a combination of advantages helps to solve the problem of replacing traditionally used internal combustion engines with electric cars, as well as hybrid and hydrogen cars.
In addition, the use of wind turbines requires the study and accounting of various wind indicators, determined by the results of multi-year observations:
- Annual and monthly average wind speeds;
- Frequency of wind speed and direction during the year, month, day;
- gustiness, calm, and maximum wind speed;
- its changes with altitude, and others.

Many factors must also be studied and considered in order to use solar energy. So, controlling the degree of polarization of ferroelectrics to produce additional energy is mainly determined by the following:
- The modification of ferroelectrics and the electrical connection scheme;
- mechanical loading (design features of the EU);
- interlayer or dipole polarization of ferroelectrics in the range of operating temperatures, as well as frequencies in the range of about 1...1.5 (103 - 105) H.The technology has no analogues. Engineering-physical solutions (innovations) have been applied. The technical details of the innovation have not been disclosed yet, since work is underway to improve the technology. The main components of the EU are protected by copyright certificates and patents, and their performance is confirmed by experimental studies. The efficiency of EU application is being studied for hydrogen and hybrid cars, as well as for increasing the energy density of batteries used for electric energy storage.

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