

Analysis of Silicon Mach Zehnder Modulator with Plus-Shaped PN Junction Phase Shifter design for Data Centre Applications

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Abstract—Nowadays, photonic devices measuring is the investigation of interest to satisfy the development of dangerous requirements at data centres. The phase shifter (PS) performance is computed the modulator performance. In this manuscript, the plus-shaped PN junction PS is deemed. This model is enhanced the modulation efficiency (ME) as well as decreased optical loss for higher-speed data rate (DR). To get greater efficiency of modulation, the P doped region width and the thickness of doped regions are differ under slabs. The simulation analysis of circuit-level is executed in the proposed PS acquired at travelling wave electrode (TWE) silicon Mach Zehnder modulator (SMZM). In 80 Gbps, the 12.39 dB maximal extinction ratio along 8.67×10^{-8} bit error rate (BER) was acquired in $V\pi L$ of 1.05 V.cm for 3.5 mm PS length. The measured intrinsic 3 dB bandwidth denotes ~ 38 GHz, whereas energy per bit transmission denotes 1.71 pJ/bit. More examines are carried out to recognize the maximal communication distance using proposed PS under SMZM for the requirements of data centre.

Keywords—PN junction PS, SMZM, bit error rate, silicon photonic device, data centre.

1. Introduction

Technological advances, like 5G, Internet of Things (IoT), Artificial Intelligence (AI) have led the way for increasing internet traffic (IT). IT is developing an alarm rate owing to enhance the file sharing, video calls and streaming, online conferences etc [1]. This increasing IT has force on data centres to implement such demands. The union of international telecommunication has issued procedures governing the use of optical bandwidth. The technology of Silicon photonics (SiPh) is suggested to fulfil the requirement of futuristic network. SiPh offers a cost-effective mode for incorporating the electronic with photonic modules at Si chip by the benefits of CMOS fabrication technology [2] & [3].

The optical modulator is a noteworthy part for higher-speed data transmission connection amid the electronic and optic mechanisms [4 -6]. Materials along hybrid optical modulators, viz Indium Tin Oxide [7 - 13] offer maximal proficiency of modulation, but it is not compatible CMOS fabrication like silicon. At silicon optical modulators, the modulation imitates the major

plasma scattering effect. In the doped region, a carrier concentration is caused by external voltage bias that leads to effectual difference of index [14]. The carrier injection (CI) and carrier depletion (CD) are occurred through forward and reverse bias voltage respectively, which is utilized the standard plasma scattering strategies. Lesser 3dB bandwidth is a major drawback of CI strategy, because maximal capacity of dispersion junction, long lifespan of free-carrier, acquired maximal ME (low $V\pi L$) [4]. The CD strategy handles this shortcoming, also aids higher-speed data process [15] & [16]. The drawback of CD is less ME (high $V\pi L$). The obtainable Mach Zehnder modulator (MZM) is chosen to its thermal stability, simple fabrication, and higher efficiency amid the optical modulators. Consuming maximal power with huge footprint is the drawback of MZM [17].

The efficiency of modulator depends upon the effective of PS utilizing doping pattern and concentration. By utilizing doping pattern, the PS is categorized as interleaved, horizontal, vertical [18 - 25]. Multi-PN junction including PS length presents greater modulation proficiency at interleaved type PS but in fabrication complexity cost. Horizontal type PS reduced the

fabrication complexity, then used lesser doping concentration in PS length cost. The PS length is lessened in vertical type depending on high doping concentrated vertical slabs. Along the carrier concentration increment, increases the free carrier absorption loss. Slot like structures are employed [26 – 28] to loss minimize, but maximize the interaction of light-object. TWE is selected on combined structure, owing to its independent of RC time stable. It helps CD technique [29–31] for getting huge footprint.

Through diminishing the doping region, the merits of horizontal with vertical mode doping is utilized at PS. Therefore, in this manuscript, a plus-shaped PN junction PS model along higher ME is proposed. The device structure is delineated in segment II. The aim is to create an optimum CD type plus-shaped PS including lesser $V\pi L$. Silicon MZM including proposed PS can satisfy the higher-speed data transmission requirement on the applications of inter with intra data centre. The experimental outcomes have been assessed in segment III.

2. Device Structure

Rib waveguide and 500nm width (W_{rib}), thick of ridge 220nm (t_{rib}), 90nm etching deepness has been deemed because it provides good optical confinement along the functioning of single-mode (TE_1), also this is a standards of fabrication.

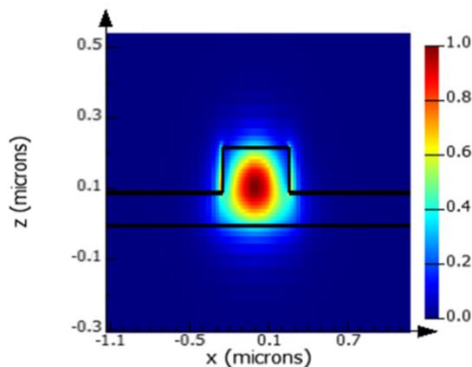


Figure 1: propagation of light via rib waveguide (500×220 nm)

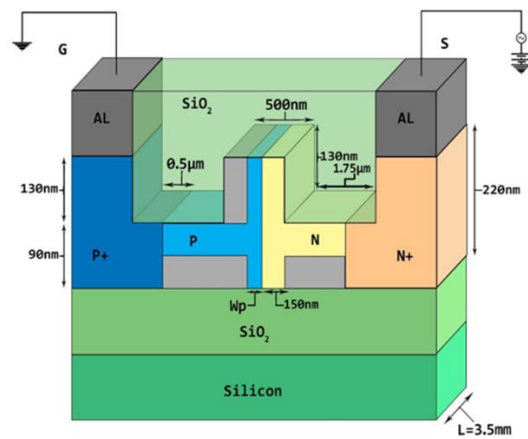


Figure 2: 3 dimensional view of plus-shaped PS

The simulation is carried out in analytical mode [32]. Figure 1 depicts the light propagation via a rib waveguide. From the waveguide centre 100nm offset is imitated to PN junction for improving the efficiency of phase. The N doped region width is set as 150nm, thickness of (P, N) slabs set as 70nm. The concentrations of P as well as N doped set to $9 \times 10^{17} \text{ cm}^{-3}$ and $7 \times 10^{17} \text{ cm}^{-3}$, because holes contain huge shift index with lesser absorb than electrons [7]. At the edge of waveguide, slab resistance has been diminished to $1 \times 10^{19} \text{ cm}^{-3}$ carrier concentration of P+ together with N+ doped region. Aluminium electrodes (Al) have been employed into electrical contacts. The PS (L) length is set as 3.5mm. Figure 2 depicts 3 dimensional view of plus-shaped PS. Maximal 5 V driving voltage is utilized to cathode ($V = 0$ to 5V) for maintaining minimal power consumption.

3. Result Analysis

The analysis was categorized as 2 level simulation: (i) device (ii) system (Figure 3). On device-state, the electro-optic as well as RF behaviour of PS is carried out with the help of finite-difference eigenmode (FDE) evaluation (Figure 3.a). In system-level, the PS parameters design is derived from MZM (PS-MZM) in Lumerical Interlink (Figure 3.b). The long-distance transmission as well as higher-speed DR is implemented for examining the proficiency of PS-MZM's to the application of data centre on and off-chip transmission.

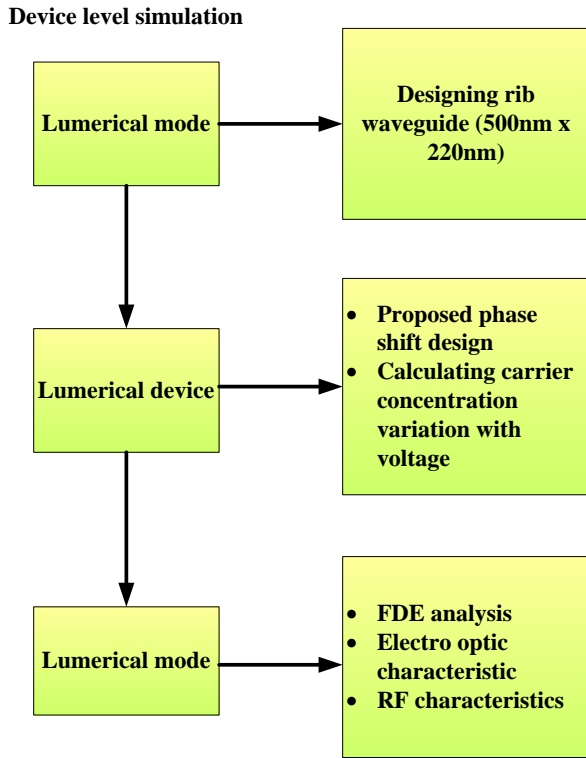


Figure 3:Simulation flow for result analysis (a) Device-level simulation

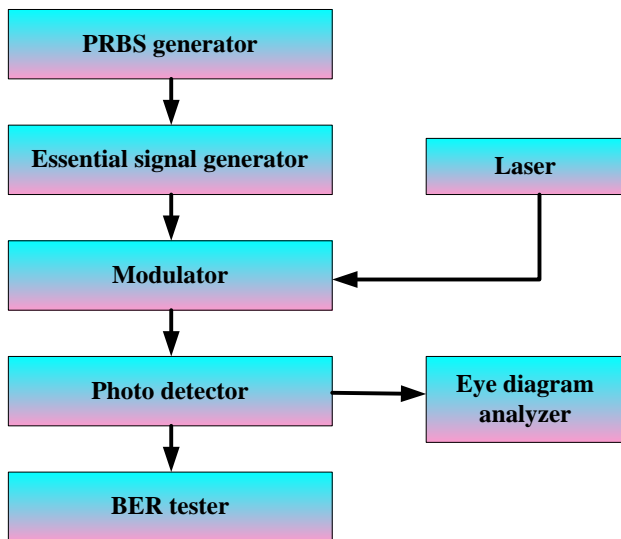


Figure 3: Simulation flow for result analysis (b) System-level simulation

3.1 Assessment of Device level

The reverse bias voltage(BV) of PS is varies for analysing the electro-optic PS performance. When BV is maximized, the carriers have been depletion from PN junction. It diminishes the density of carrier, so diminished the junction capacitance that is

represented at Figure 4. The junction capacitance (C) depending upon electron (N_n), density (1), hole (N_p).

$$C = \frac{t_{rib} \times \sqrt{(q \epsilon_0 \epsilon_r)}}{\sqrt{(2(N_p^{-1} + N_n^{-1}) \times (V_p - V))}} \quad (1)$$

Here, q implicates electric charge, ϵ_0 specifies dielectric constant, ϵ_r as relative permittivity, V_p as dispersion capacity.

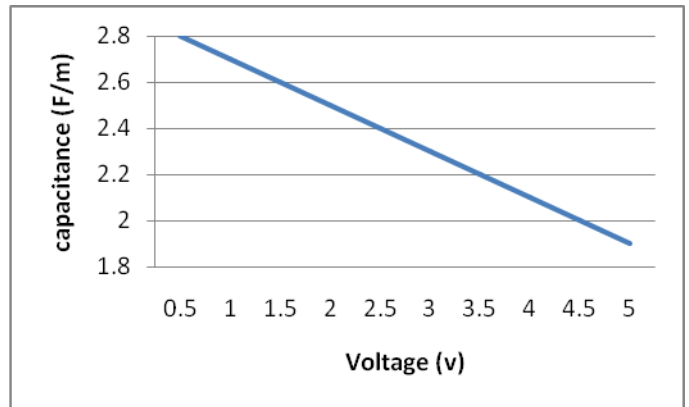


Figure 4: Junction Capacitance of PS for varying BV

CD is the impact of refractive index (Δn), absorption coefficient ($\Delta \alpha$) of PS. The derivation (2) and (3) is exhibited by Soref and Bennett [14].

$$\Delta n = -8.8 \times 10^{-22} N_n - 8.5 \times 10^{-18} N_p^{0.8} \quad (2)$$

$$\Delta \alpha = 8.5 \times 10^{-18} N_n + 6 \times 10^{-18} N_p \quad (3)$$

The optical PS feature is modified by effectual index change (5) and voltage ($\Delta n_{eff}(V)$). It occurs phase shift (φ) at propagating optical wave (OW) including PS length (L), which is exhibited in (6).

$$n_{eff}(V) = n_{eff,i} + \int \Delta n(V) dV \quad (4)$$

Here, $n_{eff,i}$ implies effectual waveguide index without doping.

$$\Delta n_{eff}(V) = n_{eff}(V) - n_{eff}(0) \quad (5)$$

$$\varphi(V) = \frac{2\pi \Delta n_{eff}(V)}{\lambda L} \quad (6)$$

The absorption coefficient α with PS (z-axis) is ,

$$\alpha(k) = \frac{\iint \Delta \alpha(V) |E(x,y,z)|^2 dx dy}{\iint |E(x,y,z)|^2 dx dy} \quad (7)$$

Here, x, y implies coordinates of waveguide dimension, z specifies length coordinate of PS, $E(x, y, z)$ signifies waveguide mode optical supply of intensity.

The absorption loss (AL) is the noteworthy part of overall loss in PS. Owing to the photons absorption via carriers, the AL is occurred (free carrier loss of absorption). As the voltage increases, the carriers drop from the junction, it lessens the carrier AL with PS. (Figure 5). The free carriers are higher while P doped region (W_p) is huge, so the loss is high via PS is acquired in lesser voltages. If the region of P doped is tiny, then decreases the loss. The necessary PS derived in maximal voltage owing to lesser variation of carrier concentration. It derives $W_p = 100\text{nm}$ a minimal loss, then needed π PS is acquired within the limits of voltage set. If diminishing $W_p < 100\text{nm}$, then the loss diminishes in the cost of phase efficient. The necessary PS to modulation is derived in 3.05V ($V\pi$) reverse bias voltage at presented structure along 4.1 dB loss. Figure 6 depicts the $V\pi$ difference including loss of PS length operation. $V\pi$ lessens the propagation OW has visible for change the Phase shift of entire PS length with maximizing length. If maximizing the carriers communication, optical mode, length, then maximizes the loss, length, but minimizes the speed of operating. It creates trade-off stage amid the $V\pi$ and PS distance.

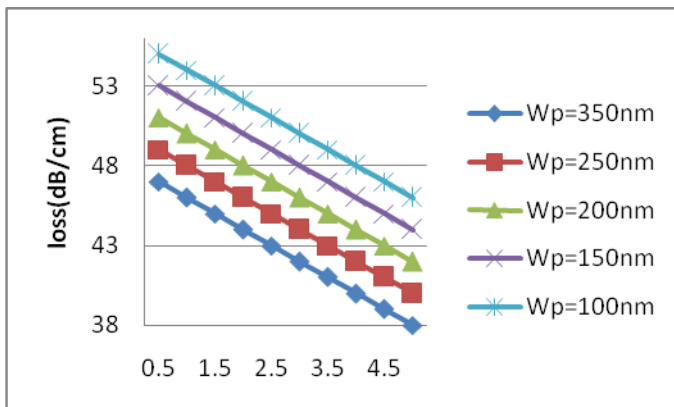


Fig 5: Loss Vs voltage to vary W_p at the presented design

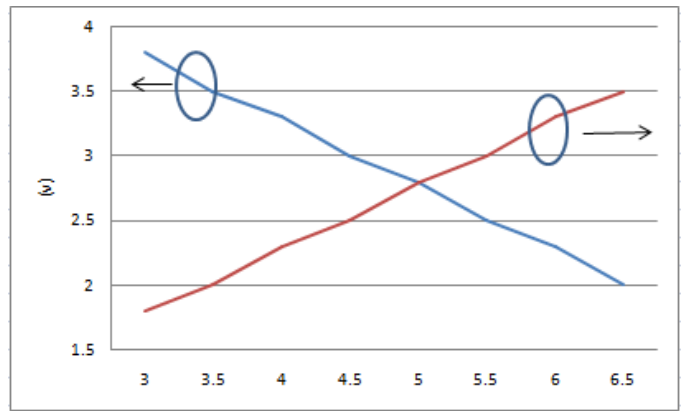


Figure 6: $V\pi$ including loss variation depending on PS length for proposed PS design along $W_p = 100\text{nm}$

The 3dB intrinsic bandwidth ($f_{3dB} = \frac{1}{2\pi RC}$) of PS is determined as 37.7GHz . Here, TWE is suggested for dealing the stable RC time, then strongly connect the RF microwave including OW. To robust connect, optical group index (OGI) must be equivalent to effectual index in specific frequency. In 26GHz , assume the index match, it leads to maximal link amid the mode of RF and optical. Figure 7 portrays the loss of 3 dB/cm determines in 26GHz . Here, loss is directly proportional to the frequency of microwave. To 3.5mm length design, 6dB bandwidth of 24.75GHz is reached (Figure 8), also assures that the device is deemed to the communication of higher-speed DR.

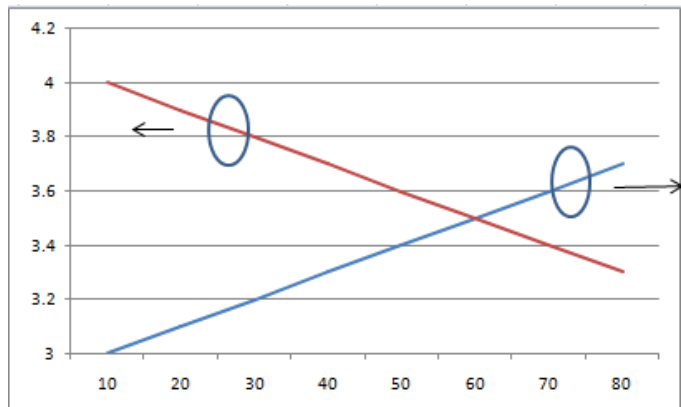


Figure 7: RF effectual index with Loss obtained depending on frequency

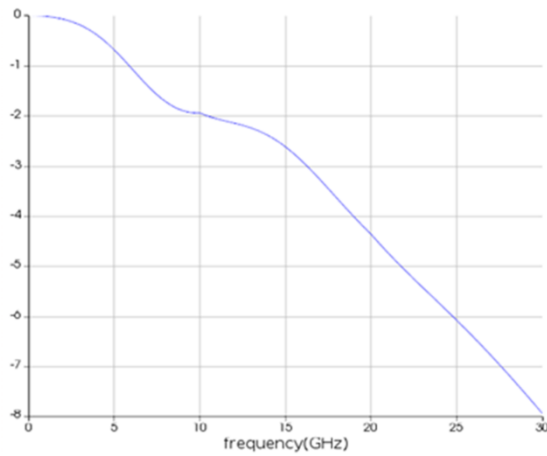


Figure 8: Electrical S21 (dB) utilizing frequency

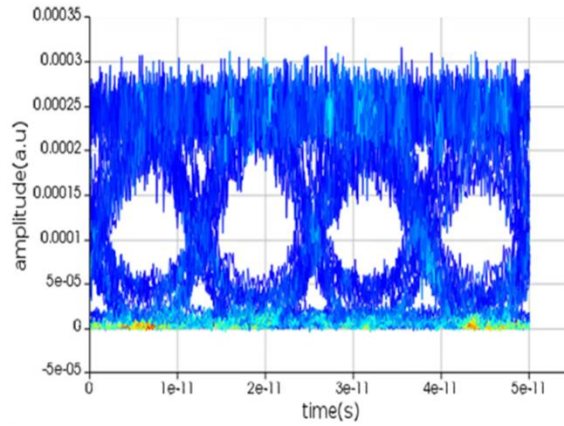


Figure 9: Eye diagram of PS-MZM and $V\pi L = 1.05V.cm$

3.2 System-level performance

Here, the dynamic performance of imbalanced MZM combined to PS design is described. PS-MZM contains 100 μm deliberate length dissimilarity including long arm, which provides 0.5V fixed bias voltage as well as irregular voltage swing (V_{pp}) and direct current reverse bias (V_{dc}) are employed to another arm. At 80Gbps, the generator of pseudo-random bit sequence (PRBS) creates a communication data. The electrical signal producer and NRZ line coding method were utilized for converting logical data as electric signal message. The 1552.5nm carrier signal is created by CW Laser. Demodulate the acquired modulated signal utilizing photodetector responsivity and $1A/W$. BER including eye diagram is assessed the signal of demodulated. Here, 12.39dB for eye diagram including extinction ratio (ER), 8.67×10^{-8} for BER, 1.05V.cm for $V\pi L$ attains $3V_{pp}$, $1.5V_{dc}$. The eye-crossing is approximately 50% as well as broad eye opening guides to the deviation of minimal duty cycle with minimal inter-code interfering. It assures the PS-MZM is appropriate for higher-speed DR utilizations. The usage of energy per bit ($E_{bit} = \frac{CV^2}{4}$) to data transfer is determined as 1.71pJ/bit. The proficiency of presented method is likened to the published articles result that is tabulated in Table 1.

Table 1: Published result's parameter comparison

Ref	L (mm)	Gbps	$V\pi L$ (V.cm)	ER (dB)
[19]	0.75	40	1.5	7.01
[20]	8	-	3.1	18
[23]	1.5	112	2.3	-
[24]	5	100	2.5	5.5
[25]	3	10	1.08	11
[26]	1.2	100	0.74	2.4
This work	3.5	80	1.05	12.3

Greater ER is derived [20] through raising the length of PS. At [24], 5mm PS length has been utilized forgetting the π phase shift and 5.5dB ER. Diminished the length to 1.2 mm [27] but requires the reverse BV approximately 6V, also 2.4dB of ER has been acquired. Table 1 displays the PS in MZM works excellent likened to different published outcomes.

Upto 15km length of data centres span have been linked through fibre optic cables. The PS-MZM efficacy to communicate amid chips coupled utilizing fibre optic cables. In 80Gbps, $\lambda = 1552.5nm$, the proficiency of transmission distance is assessed. Figure 9 represents forward error correction (FEC) threshold of bit error rate 1×10^{-3} (among chips) that PS-MZM could transfer upto 29km. It assures PS-MZM is appropriate to intra data centre utilizations along wave transmission of guided (optical fibre) with unguided (free space optics). The transmission length is maximized utilizing amplifier.

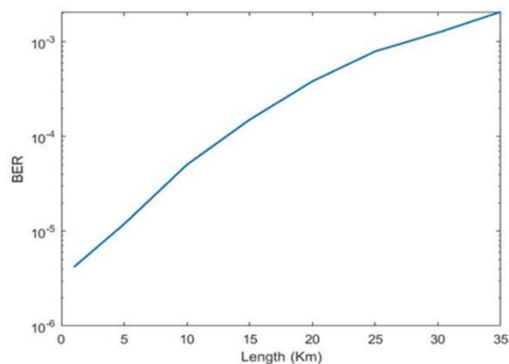


Figure 10: Transmission proficiency of PS-MZM on fibre optic cable at 80 Gbps

The speed capability of PS-MZM is deemed through changing the bit rate, then computes the BER. With maximizing bit rate, BER maximizes as inferred from figure 10. Here, PS-MZM aids to 95Gbps. The bit rate is increased by enhancing the responsivity of PIN photorecognizers or presenting the filter.

4. Conclusion

This manuscript proposes 3.5mm length plus-shaped PN junction PS for attaining greater efficacy of modulation. At the proposed design, P doped region width on rib attains 100nm, thickness of P, N doped slab regions attains 70nm. In 80 Gbps, the PS with SMZM, an ER of 12.39 dB as well as 8.67×10^{-8} BER acquires in 1.05 V.cm $\sqrt{\pi L \pi}$ for the wavelength of 1552.5 nm. The modulator is structured for fulfilling the data centre futuristic requirements, also utilized in another utilizations, viz optical switches. The PS in MZM is examined to its associate distance (29 km for inter with intra data centre interlink communication without amplifier). With the help of complex modulation modes, more enhancements in bit rate is derived.

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